Optimizing the perfectly matched layer

by F. Collino, P. B. Monk

Norbert Stoop

Overview

- PML constructed using a change of variables
 - Cartesian coordinates (review)
 - Comparison to Bérenger's approach in cylindrical coordinates
- Discretization of PMLs and resulting effects
- Optimization of cartesian PMLs
- Effects of boundary conditions

Framework: Planar Maxwell equations

PML construction - Overview

We have already seen that a PML can be understood in two ways:

- Split the magnetic field and introduce a damping term σ (Bérenger's approach)
- Perform a complex change of variables

We will see:

- 1. cartesian case: both are equivalent
- 2. cylindrical coordinates: inequivalent, efficiency differs

Planar PML for cartesian coords

Consider a TE wave ($E_z = 0$) in free space ($\epsilon_0 = \mu_0 = c = 1$). The two-dimensional Maxwell equations then reduce to:

$$\frac{\partial H_z}{\partial t} = \frac{\partial E_x}{\partial y} - \frac{\partial E_y}{\partial x}$$
$$\frac{\partial E_y}{\partial t} = -\frac{\partial H_z}{\partial x} \quad , \quad \frac{\partial E_x}{\partial t} = \frac{\partial H_z}{\partial y}$$

Suppose we'd like to construct a 2D PML for x > 0:



Bérenger PML for cart. coords

Bérenger:

1. Split *H* field: $H_z = H_{zx} + H_{zy}$ such that the MW equations can be written as:

$$\frac{\partial H_{zx}}{\partial t} = -\frac{\partial E_y}{\partial x} \quad , \quad \frac{\partial H_{zy}}{\partial t} = \frac{\partial E_x}{\partial y}$$
$$\frac{\partial E_y}{\partial t} = -\frac{\partial H_z}{\partial x} \quad , \quad \frac{\partial E_x}{\partial t} = \frac{\partial H_z}{\partial y}$$

2. Introduce damping term $\sigma(x)$ ($\sigma(x) = 0$ for x < 0) in all equations which contain *x*-derivatives:

$$\frac{\partial H_{zx}}{\partial t} + \sigma(x)H_{zx} = -\frac{\partial E_y}{\partial x} \quad , \quad \frac{\partial H_{zy}}{\partial t} = \frac{\partial E_x}{\partial y}$$
$$\frac{\partial E_y}{\partial t} + \sigma(x)E_y = -\frac{\partial H_z}{\partial x} \quad , \quad \frac{\partial E_x}{\partial t} = \frac{\partial H_z}{\partial y}$$

Bérenger PML for cart. coords II

3. In time harmonic regime,

$$E_i(x, y, t) = \hat{E}_i(x, y) \exp(-i\omega t), \quad H_{zi}(x, y, t) = \hat{H}_{zi}(x, y) \exp(-i\omega t), \quad i = x, y$$

the PML equations can be written as:

$$\begin{split} -i\omega\hat{H}_z &= \frac{\partial\hat{E}_x}{\partial y} - \frac{1}{1+i\sigma/\omega}\frac{\partial\hat{E}_y}{\partial x},\\ -i\omega\hat{E}_y &= -\frac{1}{1+i\sigma/\omega}\frac{\partial\hat{H}_z}{\partial x}, \qquad -i\omega\hat{E}_x = \frac{\partial\hat{H}_z}{\partial y} \end{split}$$

Change of variables technique

1. Start again in time harmonic regime, but don't split fields:

$$E_i(x, y, t) = \hat{E}_i(x, y) \exp(-i\omega t), \quad H_z(x, y, t) = \hat{H}_z(x, y) \exp(-i\omega t), \quad i = x, y$$

2. In frequency domain, the Maxwell equations become:

$$\begin{aligned} -i\omega\hat{H}_z &= \frac{\partial\hat{E}_x}{\partial y} - \frac{\partial\hat{E}_y}{\partial x}, \\ -i\omega\hat{E}_y &= -\frac{\partial\hat{H}_z}{\partial x}, \quad -i\omega\hat{E}_x = \frac{\partial\hat{H}_z}{\partial y} \end{aligned}$$

3. Change of variables: $x \to x' = x + \frac{i}{\omega} \int_0^x \sigma(s) ds$

Change of variables technique II

If we use the chain rule to replace x' by x, we get:

$$-i\omega\hat{H}_{z} = \frac{\partial\hat{E}_{x}}{\partial y} - \frac{1}{1+i\sigma/\omega}\frac{\partial\hat{E}_{y}}{\partial x},$$
$$-i\omega\hat{E}_{y} = -\frac{1}{1+i\sigma/\omega}\frac{\partial\hat{H}_{z}}{\partial x}, \quad -i\omega\hat{E}_{x} = \frac{\partial\hat{H}_{z}}{\partial y}$$

This is exactly the Bérenger PML in the frequency domain: **Both** approaches are equivalent!

Practical computation: truncate PML. We impose Dirichlet BC:

$$\hat{E}_y(x=\delta,y,t)=0 \implies R=e^{-2ik_x\int_0^\delta(1+i\sigma(s)/\omega)ds}$$

Note: Pick σ large to minimize R (if $k_x \in \mathbb{R}$).

PML for curvilinear coordinates

Do Bérenger's and the complex change of variables approach also result in equivalent PMLs for non-Cartesian coordinate system? Maxwell's equations in polar coordinates (ρ , θ):

$$\frac{\partial H_z}{\partial t} = \frac{1}{\rho} \left(\frac{\partial E_{\rho}}{\partial \theta} - \frac{\partial}{\partial \rho} (\rho E_{\theta}) \right)$$
$$\frac{\partial E_{\rho}}{\partial t} = \frac{1}{\rho} \frac{\partial H_z}{\partial \theta}, \quad \frac{\partial E_{\theta}}{\partial t} = -\frac{\partial H_z}{\partial \rho}$$

Assume the layer starts at $\rho = a$, so $\sigma(\rho) > 0$ for $\rho > a$ and 0 otherwise.



Change of variables for polar coords

Start in the frequency domain. Let $\rho' = \rho + \frac{i}{\omega} \int_a^{\rho} \sigma(s) ds$ and introduce

$$d(\rho) = 1 + i \frac{\sigma(\rho)}{\omega}$$
 and $\bar{d}(\rho) = 1 + i \frac{1}{\rho \omega} \int_{a}^{\rho} \sigma(s) ds$

such that $\rho' = \rho \overline{d}$ and $\frac{d\rho'}{d\rho} = d$. We thus have in freq. domain:

$$-i\omega H_z = \frac{1}{\bar{d}\rho} \left(\frac{\partial E_{\rho}}{\partial \theta} - \frac{1}{d} \frac{\partial}{\partial \rho} (\bar{d}\rho E_{\theta}) \right)$$
$$-i\omega E_{\rho} = \frac{1}{\bar{d}\rho} \frac{\partial H_z}{\partial \theta}, \quad -i\omega E_{\theta} = -\frac{1}{d} \frac{\partial H_z}{\partial \rho}$$

Note: $\frac{1}{d} \frac{\partial}{\partial \rho} = \frac{\partial}{\partial \rho'} = \frac{\partial}{\partial (\bar{d}\rho)}$

Change of variables for polar coords II

Using $\tilde{E}_{\rho} = dE_{\rho}$ and $\tilde{E}_{\theta} = \bar{d}E_{\theta}$ we get the traditional Helmholtz equations:

$$\begin{split} -i\omega d\bar{d}H_z &= \frac{1}{\rho} \left(\frac{\partial \tilde{E}_{\rho}}{\partial \theta} - \frac{\partial}{\partial \rho} (\rho \tilde{E}_{\theta}) \right) \\ -i\omega \frac{\bar{d}}{d} \tilde{E}_{\rho} &= \frac{1}{\rho} \frac{\partial H_z}{\partial \theta}, \quad -i\omega \frac{d}{\bar{d}} \tilde{E}_{\theta} = -\frac{\partial H_z}{\partial \rho} \end{split}$$

We can return to time domain by introducing $E_{\rho}^* = 1/d\tilde{E}_{\rho}$, $E_{\theta}^* = 1/d\tilde{E}_{\theta}$, $H_z^* = \bar{d}H_z$ and $\bar{\sigma}(\rho) = \frac{1}{\rho} \int_a^{\rho} \sigma(s) ds$:

$$\frac{\partial H_z^*}{\partial t} + \sigma H_z^* = \frac{1}{\rho} \left(\frac{\partial \tilde{E}_{\rho}}{\partial \theta} - \frac{\partial}{\partial \rho} (\rho \tilde{E}_{\theta}) \right), \quad \frac{\partial E_{\rho}^*}{\partial t} + \bar{\sigma} E_{\rho}^* = \frac{1}{\rho} \frac{\partial H_z}{\partial \theta}, \quad \frac{\partial E_{\theta}^*}{\partial t} + \sigma E_{\theta}^* = -\frac{\partial H_z}{\partial \rho}$$
$$\frac{\partial \tilde{E}_{\rho}}{\partial t} = \frac{\partial E_{\rho}^*}{\partial t} + \sigma E_{\rho}^*, \quad \frac{\partial \tilde{E}_{\theta}}{\partial t} = \frac{\partial E_{\theta}^*}{\partial t} + \bar{\sigma} E_{\theta}^*, \quad \frac{\partial H_z}{\partial t} + \bar{\sigma} H_z = \frac{\partial H_z^*}{\partial t}$$

Comparison to Bérenger's PML

In order to compare the two constructions, assume that $\frac{\partial H_z}{\partial \theta} = 0$ and choose $E_{\rho} = 0$.

$$\implies \frac{\partial H_z^*}{\partial t} + \sigma H_z^* = -\frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho \tilde{E}_\theta), \qquad \frac{\partial E_\theta^*}{\partial t} + \sigma E_\theta^* = -\frac{\partial H_z}{\partial \rho}$$
$$\frac{\partial \tilde{E}_\theta}{\partial t} = \frac{\partial E_\theta^*}{\partial t} + \bar{\sigma} E_\theta^*, \qquad \frac{\partial H_z}{\partial t} + \bar{\sigma} H_z = \frac{\partial H_z^*}{\partial t}$$

Bérenger's construction would yield:

$$\frac{\partial H_z}{\partial t} + \sigma H_z = -\frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho E_\theta), \qquad \frac{\partial E_\theta}{\partial t} + \sigma E_\theta = -\frac{\partial H_z}{\partial \rho}$$

They are clearly different!

Question: How do they perform qualitatively?

Comparison to Bérenger's PML II

Think of the following setup:



We take the source to be on the unit disc,

At $\rho = 1$: $E_{\theta} = \sin(2\pi t)$ for $0 \le t \le 1$ and 0 otherwise,

and choose a quadratic ρ -dependence for σ :

$$\sigma(\rho) = \sigma_0(\rho - a)^2/\delta^2$$
, for $\rho \ge a$

Comparison to Bérenger's PML III



Conclusions

- The change of variables PML gives a much more accurate (discrete) absorbing layer than Bérenger's construction in polar coordinates.
- Unlike Bérenger's PML, the change of variables technique allows tuning of PMLs situated very close to the scatterer, yet producing very good absorption.
- The quality of our PML still depends on a number of parameters (including discretization params) which need to be chosen wisely.

 \implies Is there a way to quantify the effects of discretization? Furthermore, can we derive optimal PML parameters from there?

Effects of discretization

For simplicity, we restrict ourselves to the planar, two-dimensional case. Starting from Bérenger's construction, we avoid the split fields by defining:

$$\tilde{E}_x = (1 + i\sigma/\omega)\hat{E}_x, \quad \tilde{E}_y = \hat{E}_y, \quad \tilde{H}_z = \hat{H}_z$$

Now we have again a traditional curl-curl structure:

$$-i\omega(1 - i\sigma/\omega)\tilde{H}_z = \frac{\partial\tilde{E}_x}{\partial y} - \frac{\partial\tilde{E}_y}{\partial x}$$
$$-i\omega(1 - i\sigma/\omega)\tilde{E}_y = -\frac{\partial\tilde{H}_z}{\partial x}, \qquad -\frac{i\omega}{1 + i\sigma/\omega}\tilde{E}_x = \frac{\partial\tilde{H}_z}{\partial y}$$

Discretization of planar PML

We use

a standard Yee scheme and let $\sigma(x)$ be piecewise constant with jumps at x = lh, $l = 0, 1, 2, \ldots$ We denote by $\sigma_{l+1/2}$ the value of σ in the interval (lh, (l+1)h).

We then arrive at the following discretized equations:



$$\begin{split} -i\frac{\omega}{\gamma_{l+1/2}}\tilde{E}_{l+1/2,j} &= \frac{H_{l+1/2,j+1/2} - H_{l+1/2,j-1/2}}{h} \\ -i\omega\frac{\gamma_{l+1/2} + \gamma_{l-1/2}}{2}\tilde{E}_{l,j+1/2} &= -\frac{\tilde{H}_{l+1/2,j+1/2} - \tilde{H}_{l-1/2,j+1/2}}{h} \\ -i\omega\gamma_{l+1/2}\tilde{H}_{l+1/2,j+1/2} &= \frac{\tilde{E}_{l+1/2,j+1} - \tilde{E}_{l+1/2,j}}{h} - \frac{\tilde{E}_{l+1,j+1/2} - \tilde{E}_{l,j+1/2}}{h} \end{split}$$

with $\gamma_{l+1/2} = 1 + i\sigma_{l+1/2}/\omega$.

Discretization of planar PML II

To make life easier: Assume $\tilde{H}_{l+1/2,j+1/2} = e^{i\kappa_2(j+1/2)h}\tilde{H}_{l+1/2}$ and eliminate the various \tilde{E} 's to get an expression for \tilde{H} only:

$$-h^{2}\omega^{2}\lambda\gamma_{l+1/2}\tilde{H}_{l+1/2} = \frac{2}{\gamma_{l+3/2}+\gamma_{l+1/2}}(\tilde{H}_{l+3/2}-\tilde{H}_{l+1/2}) \\ -\frac{2}{\gamma_{l+1/2}+\gamma_{l-1/2}}(\tilde{H}_{l+1/2}-\tilde{H}_{l-1/2})$$

where we defined $\lambda = 1 - \frac{4}{h^2 \omega^2} \sin^2(\kappa_2 h/2)$.

To find the reflection coefficient due to the discretization, we'll use $\sigma = const$, thus $\gamma = \gamma_{l+1/2} = const$ and use the plain wave ansatz

$$\begin{split} \tilde{H}_{l+1/2} &= e^{i\kappa_1 h(l+1/2)} + R e^{-i\kappa_1 h(l+1/2)} & \text{for } l \leq -1 \quad (x < 0) \\ \tilde{H}_{l+1/2} &= T e^{i\kappa_1^{\sigma} h(l+1/2)} & \text{for } l \geq 0 \text{ (inside PML)} \end{split}$$

Discretization of planar PML III

Using this ansatz to solve the discrete \tilde{H} equations at the interface (corresponding to x = 0), we can derive an expression for the reflection coeffcient R for an *infinite* layer:

$$R = \frac{1}{16}(\omega^{2} - \kappa_{2}^{2})\frac{\sigma(\sigma - 2\omega i)}{\omega^{2}}h^{2} + O(h^{4})$$

Discretizing the PML has introduced a reflection from the interface at x = 0.

The layer is thus no longer perfectly matched . As *R* is of magnitude $\sigma^2 h^2$, we cannot choose σ arbitrarily large anymore.

Before dealing with an optimal choice of σ , we will consider the case of a *finite* layer.

Refl. coeff. for fi nite, discrete PMLs

Suppose a PML thickness of $\delta = n_l \cdot h$. The discretized equations at $l = n_l - 1$ will require the value of the boundary data. If we choose Dirichlet BC, we can set $\tilde{E}_{n_l,j+1/2} = 0$, $\forall j$. Remember:

$$-i\omega\gamma\tilde{E}_{n_{l},j+1/2} = -\frac{\tilde{H}_{n_{l}+1/2,j+1/2} - \tilde{H}_{n_{l}-1/2,j+1/2}}{h},$$

$$-h^{2}\omega^{2}\lambda\gamma\tilde{H}_{l+1/2} = \frac{1}{\gamma}(\tilde{H}_{l+3/2} - \tilde{H}_{l+1/2}) - \frac{1}{\gamma}(\tilde{H}_{l+1/2} - \tilde{H}_{l-1/2})$$

Given $\tilde{H}_{-3/2}$, we can therefore compute

$$\vec{H} = (\tilde{H}_{-1/2}, \tilde{H}_{1/2}, \dots, \tilde{H}_{n_l-1/2})^{\top}$$

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Refl. coeff. for fi nite, discrete PMLs II

It is easier to calculate \vec{H} in terms of the matrix equation

$$M\vec{H} = -\tilde{H}_{-3/2}\vec{F}$$

where
$$\vec{F} = (1, 0, \dots, 0)^{\top}$$
 and $M = \begin{pmatrix} c_{-1/2} & d_{1/2} & 0 & \dots & \\ d_{1/2} & c_{1/2} & d_{3/2} & 0 & \dots & \\ 0 & d_{3/2} & c_{3/2} & d_{5/2} & \dots & \\ & \ddots & \ddots & \ddots & \ddots & \\ & \dots & 0 & d_{n_l-3/2} & c_{n_l-1/2} \end{pmatrix}$

with

$$c_{j+1/2} = h^2 \omega^2 \lambda \gamma_{j+1/2} - \frac{2}{\gamma_{j+3/2} + \gamma_{j+1/2}} - \frac{2}{\gamma_{j+1/2} + \gamma_{j-1/2}}, \quad -1 \le j \le n_l - 2$$

$$d_{j+1/2} = 2/(\gamma_{j+1/2} + \gamma_{j-1/2}), \quad 0 \le j \le n_l - 1,$$

$$c_{n_l-1/2} = h^2 \omega^2 \lambda \gamma_{n_l-1/2} - 2/(\gamma_{n_l-1/2} + \gamma_{n_l-3/2})$$

Refl. coeff. for fi nite, discrete PMLs III

An expression for the reflection coefficient is then given by

$$R_{dis} = -\frac{1 + F^{\top} \cdot M^{-1} \cdot F \cdot e^{-i\kappa_1 h}}{1 + F^{\top} \cdot M^{-1} \cdot F \cdot e^{i\kappa_1 h}}$$

Numerical results: We choose

$$\begin{split} \delta &= n_l h &= 2\pi/\omega & \text{(layer thickness} = 1 \text{ wavelength)} \\ \sigma(x) &= \sigma_0 (x/\delta)^2, \text{ for } x > 0 & \text{(parabolic law)} \\ \sigma_0 &= \frac{3}{2\delta} \log(\frac{1}{R_0}) & \text{(number of points per wavelength)} \end{split}$$

The choice of σ_0 ensures that the reflection coefficient for the *continuous* model at *normal incidence* is just given by R_0 (Remember: $R_{cont} = e^{-2ik_x \int_0^{\delta} (1+i\sigma(s)/\omega) ds}$ for continuous models).

Numerical results I



Numerical results II



Conclusions

- The numerical reflection coefficient converges to the derived value for the continuous model when N is increased.
- The convergence appears to be slower for smaller R_0 (ie. for larger σ_0).
- For fi xed N, the largest value of σ_0 does not necessarily result in the smallest reflection coeffi cient.

Question: Can we choose σ in a better way in order to optimize the effects introduced by discretization?

Optimization of the cart. PML

For practical reasons: For a given N (number of points per wavelength) and n_l (number of points in the layer), what is the best σ to use?

 \implies Introduce (discrete) $\vec{\sigma}$:

$$\vec{\sigma} = (h\sigma_{1/2}, h\sigma_{3/2}, \dots, h\sigma_{n_l-1/2})$$

 $\vec{\sigma}$ is then found by minimizing *R* for all angles of incidence. We can - as an example - emphasize *normal* incidence by a $\cos \theta$ weight, thus minimize

$$\frac{1}{100} \sum_{q=1}^{100} \cos(\theta_q) |R(\theta, N, \vec{\sigma})|^2,$$

where $\theta_q = \pi(q-1)/200$.

Numerical results



Optimal σ profille is not quadraticanymore.

- The optimized σ improves the average reflection coefficient.
- The improvement is best for non-normal incidence.

Effects of boundary conditions

We have already seen: Dirichlet BCs lead to additional reflections. Idea: Use absorbing boundary conditions (ABC) at the end of the PML layer:

 $\tilde{E}_y = \tilde{H}_z$ on $x = \delta$ (Silver-Müller radiation cond.)

 \Rightarrow It will clearly influence $\tilde{H}_{n_l-1/2}$.

Start with the Maxwell equation at the layer end $x = \delta = n_l h$:

$$(-i\omega + \sigma(x))\tilde{E}_y = -\frac{\partial \tilde{H}_z}{\partial x}$$

Using a special FD scheme, it can be discretized in the following form

$$-i\omega\gamma_{n_l-1/2}\tilde{E}_{n_l,j+1/2} = -\frac{\tilde{H}_{n_l,j+1/2} - \tilde{H}_{n_l-1/2,j+1/2}}{h/2}$$

Effects of boundary conditions II

But, as imposed by our boundary conditions, $\tilde{H}_{n_l,j+1/2} = \tilde{E}_{n_l,j+1/2}$, this simplifies to:

$$-i\omega h\left(\frac{\gamma_{n_l-1/2}}{2} + \frac{i}{\omega h}\right)\tilde{E}_{n_l,j+1/2} = \tilde{H}_{n_l-1/2,j+1/2}$$

We can now proceed as with Dirichlet BCs: Split away the *j* part and define $\vec{H} = (\tilde{H}_{-1/2}, \cdots, \tilde{H}_{n_l-1/2})$ and *M* such that $M\vec{H} = -\tilde{H}_{-3/2}\vec{F}$.

Due to our new boundary conditions, only the last line in M will change, corresponding to the different expression for $\tilde{H}_{n_l-1/2}$. The reflection coefficient, however, is still given by the same formula derived earlier:

$$R = -\frac{1 + F^{\top} \cdot M^{-1} \cdot F \cdot e^{-i\kappa_1 h}}{1 + F^{\top} \cdot M^{-1} \cdot F \cdot e^{i\kappa_1 h}}$$

Numerical results



Numerical results II



Conclusions

- Using ABC's the reflection coefficient converges to zero with higher accuracy. This is what we expect, since our ABC's are perfect, at least for normal wave incidence.
- For parabolic σ , the ABC's improve the reflection for waves close to normal incidence.
- Not shown: Optimizing σ for ABC's does not result in a large improvement, compared to the parabolic case.

Summarized: Absorbing boundary conditions can be considered an enhancement for parabolic σ , especially for normal incidence.

To come to an end...

We have seen that

- PMLs can be generalized to curvilinear coordinates using a complex change of variables, which is superior to Bérenger's construction.
- the effects of discretization can be quantified and we have derived an expression for the reflection coefficient for both, the infinite and the finite layer.
- in order to improve the (discrete, fi nite) layer, we can optimize σ. However, the parabolic profile is almost optimal.
- using ABC's is worth while for parabolic σ profiles. An optimized profile, however, will then not lead to great improvement.

Questions?